## **General Description**

The MAX3286/MAX3296 series of products are highspeed laser drivers for fiber optic LAN transmitters, optimized for Gigabit Ethernet applications. Each device contains a bias generator, laser modulator, and comprehensive safety features. Automatic power control (APC) adjusts the laser bias current to maintain average optical power at a constant level, regardless of changes in temperature or laser properties. For lasers without a monitor photodiode, these products offer a constant-current mode. The circuit can be configured for use with conventional shortwave (780nm to 850nm) or longwave (1300nm) laser diodes, as well as verticalcavity surface-emitting lasers (VCSELs).

The MAX3286 series (MAX3286-MAX3289) is optimized for operation at 1.25Gbps, and the MAX3296 series (MAX3296-MAX3299) is optimized for 2.5Gbps operation. Each device can switch 30mA of laser modulation current at the specified data rate. Adjustable temperature compensation is provided to keep the optical extinction ratio within specifications over the operating temperature range. This series of devices is optimized to drive lasers packaged in low-cost TO-46 headers. Deterministic jitter (DJ) for the MAX3286 is typically 22ps, allowing a 72% margin to Gigabit Ethernet DJ specifications.

These laser drivers provide extensive safety features to guarantee single-point fault tolerance. Safety features include dual enable inputs, dual shutdown circuits, and a laser-power monitor. The safety circuit detects faults that could cause dangerous light output levels. A programmable power-on reset pulse initializes the laser driver at startup.

The MAX3286/MAX3296 are available in a compact, 5mm × 5mm, 28-pin QFN package; a 5mm × 5mm, 32-pin TQFP package; or in die form. The MAX3287/MAX3288/ MAX3289 and MAX3297/MAX3298/MAX3299 are available in a 16-pin TSSOP-EP package.

**Applications** 

Gigabit Ethernet Optical Transmitter Fibre Channel Optical Transmitter ATM LAN Optical Transmitter

Typical Application Circuits and Selector Guide appear at end of data sheet.

## Features

- 7ps Deterministic Jitter (MAX3296) 22ps Deterministic Jitter (MAX3286)
- +3.0V to +5.5V Supply Voltage
- Selectable Laser Pinning (Common Cathode or Common Anode) (MAX3286/MAX3296)
- 30mA Laser Modulation Current
- Temperature Compensation of Modulation Current
- Automatic Laser Power Control or Constant Bias Current
- Integrated Safety Circuits
- Power-On Reset Signal
- QFN Package Available

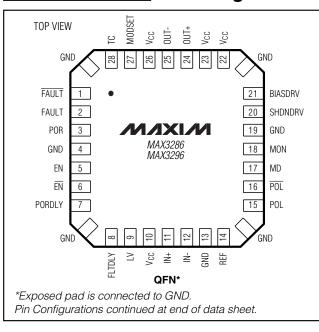
## **Ordering Information**

PART	TEMP. RANGE	PIN- PACKAGE
MAX3286CGI	0°C to +70°C	28 QFN (5mm × 5mm)**
MAX3286CHJ	0°C to +70°C	32 TQFP (5mm × 5mm)
MAX3286C/D	0°C to +70°C	Dice*

Ordering Information continued at end of data sheet.

\*Dice are designed to operate from  $T_J = 0^{\circ}C$  to +110°C, but are tested and guaranteed only at  $T_A = +25^{\circ}C$ . \*\*Exposed pad.

## **Pin Configurations**



## **M**XX/M

Maxim Integrated Products 1

For price, delivery, and to place orders, please contact Maxim Distribution at 1-888-629-4642. or visit Maxim's website at www.maxim-ic.com.

## **ABSOLUTE MAXIMUM RATINGS**

Supply Voltage at V<sub>CC</sub> .....-0.5V to +7.0V Voltage at EN, EN, PORDLY, FLTDLY, LV, IN+, IN-, REF, POL, POL, MD, MON, BIASDRV,

32-Pin TQFP (derate 14.3mW/°C above +70°C	C)1100mW
28-Pin QFN (derate 28.7mW/°C above +70°C	
16-Pin TSSOP (derate 27mW/°C above +70°C	C)2162mW
Operating Temperature Range	0°C to +70°C
Operating Junction Temperature Range	
Processing Temperature (die)	+400°C
Storage Temperature Range	-55°C to +150°C
Lead Temperature (soldering, 10s)	+300°C

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## **ELECTRICAL CHARACTERISTICS**

(V<sub>CC</sub> = +3.0V to +5.5V,  $T_A = 0^{\circ}$ C to +70°C, unless otherwise noted. Typical values are at V<sub>CC</sub> = +3.3V and  $T_A = +25^{\circ}$ C,  $R_{TC} =$ open; see Figure 1a.)

PARAMETER	SYMBOL	CONDITIONS	MIN	ТҮР	MAX	UNITS
Supply Current	Icc	Figure 1a, $R_{MOD} = 1.82k\Omega$		52	75	mA
Data Input Voltage Swing	VID	Total differential signal, peak-to-peak, Figure	200		1660	mV
TTL Input Current		$0 \le V_{PIN} \le V_{CC}$	-100		100	μΑ
TTL Input High Voltage	VIH		2.0			V
TTL Input Low Voltage	VIL				0.8	V
FAULT, FAULT Output High Voltage	V <sub>OH</sub>	I <sub>OH</sub> = -100μA	2.4			V
FAULT, FAULT Output Low Voltage	Vol	I <sub>OL</sub> = 1mA			0.4	V
BIAS GENERATOR (Note 1)					1	
BIASDRV Current, Shutdown		EN = GND	-1		1	μΑ
BIASDRV Current Sink		FAULT = low, $V_{BIASDRV} \ge 0.6V$	0.8			~^^
BIASDRV Current Source		FAULT = low, $V_{BIASDRV} \le V_{CC} - 1V$	0.8			mA
REF Voltage		$I_{REF} \le 2mA$ , MON = $V_{CC}$	2.45	2.65	2.85	V
MD Nominal Voltage	V <sub>MD</sub>	APC loop is closed	1.55	1.7	1.85	V
MD Voltage During Fault		Common-cathode configuration		0.4	1.2	V
MD voltage During Fault		Common-anode configuration	2	V <sub>CC</sub> - 0.8		v
MD Input Current		Normal operation (FAULT = low)	-2	0.16	2	μΑ
MON Input Current		V <sub>MON</sub> = V <sub>CC</sub>		0.44	6	μΑ
POWER-ON RESET			•			
POR Threshold		LV = GND	3.9		4.5	V
FOR ITTESTOID		LV = open	2.65		3.0	v
POR Hysteresis				150		mV
FAULT DETECTION			•			
REF Fault Threshold					2.95	V
MD High Fault Threshold			V <sub>MD</sub> + 59	% V <sub>M</sub>	<sub>D</sub> + 20%	
MD Low Fault Threshold			V <sub>MD</sub> - 20	% V	MD - 5%	
MON Fault Threshold		MAX3286/MAX3288/MAX3296/MAX3298	V <sub>CC</sub> - 600		V <sub>CC -</sub> 480	mV
MODSET, TC Fault Threshold					0.9	V

## **ELECTRICAL CHARACTERISTICS (continued)**

(V<sub>CC</sub> = +3.0V to +5.5V,  $T_A = 0^{\circ}C$  to +70°C, unless otherwise noted. Typical values are at V<sub>CC</sub> = +3.3V and  $T_A = +25^{\circ}C$ ,  $R_{TC} = open$ ; see Figure 1a.)

	CONDITIONS					UNITS
	1		I			
	ISHDNDRV = 10µA, F	AULT asserted	V <sub>CC</sub> - 0.4	1		
	ISHDNDRV = 15mA, FAULT not asserted		0	V	CC - 1.2	V
	ISHDNDRV = 1mA, FAULT not asserted		0	V	cc - 2.4	l
	I					1
	MAX3286 series			1.25		
	MAX3296 series			2.5		Gbps
					2	mA
	$R_L \le 25\Omega$		30			mA
	RMOD = 1.9kΩ (imor	= 30 mA	-10		10	
			-15		15	%
		MAX3286 series	-	130	220	
	20% to 80%	MAX3296 series		90	150	ps
		$R_{MOD} = 13k\Omega$		46	65	
	MAX3286 series	$R_{MOD} = 4.1 k\Omega$ (i <sub>MOD</sub> = 15mA)		29	45	-
		$R_{MOD} = 1.9 k\Omega$ ( $i_{MOD} = 30 mA$ )		22	35	
		$R_{MOD} = 13k\Omega$ (imod = 5mA)		14	35	ps
	MAX3296 series	$R_{MOD} = 4.1 k\Omega$ (i <sub>MOD</sub> = 15mA)		8	22	
		$R_{MOD} = 1.9k\Omega$ ( $i_{MOD} = 30mA$ )		7	20	
	MAX3286 series			2	8	
	MAX3296 series			2	4	ps
				15	200	μA
	Tempco = max, R <sub>M</sub> o	g = open; Figure 5		4000		
				50		ppm/°(
			620	800	980	Ω
	Single ended		42	50	58	Ω
	-			V <sub>CC</sub> - 0.3		V
	1		I			1
	PORDLY = open		0.3	1.25		μs
<b>t</b> PORDLY	$C_{PORDLY} = 0.01 \mu F,$		3	5.5		ms
teal II τ	,			22		μs
I AOLI	,,		10	20		μs
	tpordly tfault	ISHDNDRV = 15mA, F       ISHDNDRV = 1mA, F/       ISHDNDRV = 1mA, F/       MAX3286 series       MAX3296 series       RL ≤ 25Ω       RMOD = 1.9kΩ (iMOD       RMOD = 13kΩ (iMOD       20% to 80%       MAX3286 series       MAX3286 series       MAX3286 series       MAX3286 series       MAX3296 series       Single ended       Single ended       PORDLY = 001µF, MAX3286/MAX3296	$\begin{tabular}{ c                                   $			

M/X/M

## **ELECTRICAL CHARACTERISTICS (continued)**

(V<sub>CC</sub> = +3.0V to +5.5V,  $T_A = 0^{\circ}C$  to +70°C, unless otherwise noted. Typical values are at V<sub>CC</sub> = +3.3V and  $T_A = +25^{\circ}C$ ,  $R_{TC} = open$ ; see Figure 1a.)

PARAMETER	SYMBOL	CONDITIONS	MIN	ТҮР	MAX	UNITS
FLTDLY Duration		C <sub>FLTDLY</sub> = 0	0.2	1		
	<sup>t</sup> FLTDLY	$C_{FLTDLY} = 270 pF$	100	140		μs
EN or EN Minimum Pulse Width Required to Reset a Latched Fault	ten_RESET	MAX3286/MAX3296 only, Figure 1b		6	10	ns
FAULT Reset After EN, $\overline{EN}$ , or POR Transition	<b>t</b> RESET	MAX3286/MAX3296 only, Figure 1b		1	2	μs
SHDNDRV Asserted After EN = Low or EN = High	<b>t</b> SHUTDN	MAX3286/MAX3296 only, Figure 1b		3.5	5.5	μs

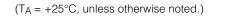
**Note 1:** Common-anode configuration refers to a configuration where POL = GND,  $\overline{POL} = V_{CC}$ , and an NPN device is used to set the laser bias current. Common-cathode configuration refers to a configuration where  $POL = V_{CC}$ ,  $\overline{POL} = GND$ , and a PNP device is used to set the laser bias current.

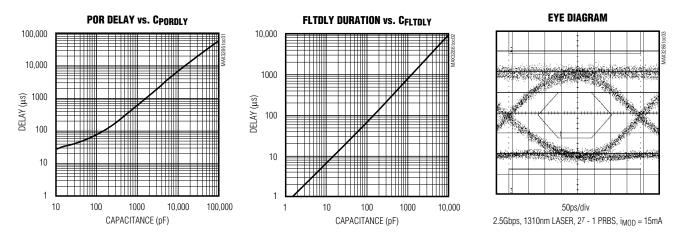
Note 2: Deterministic jitter measured with a repeating K28.5 bit pattern 0011111010100000101. Deterministic jitter is the peak-topeak deviation from the ideal time crossings per ANSI X3.230, Annex A.

Note 3: For Fibre Channel and Gigabit Ethernet applications, the peak-to-peak random jitter is 14.1 times the RMS jitter.

Note 4: Delay from a fault on MD until FAULT is asserted high.

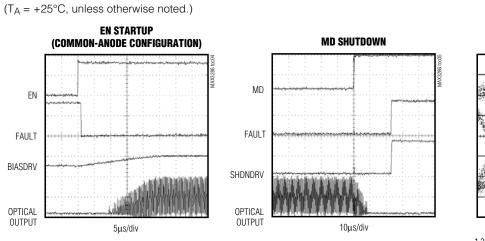
## **Typical Operating Characteristics**







## **Typical Operating Characteristics (continued)**



**EN STARTUP** 

5µs/div

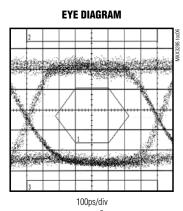
ΕN

FAULT

BIASDRV

OPTICAL

OUTPUT



1.25Gbps, 1310nm LASER, 2<sup>7</sup> - 1 PRBS, i<sub>mod</sub> = 15mA

## Pin Description

MAX3286-MAX3289/MAX3296-MAX3299

	Р	IN			
QFN MAX3286 MAX3296	TQFP MAX3286 MAX3296	TSSOP-EP MAX3287 MAX3297 MAX3289 MAX3289 MAX3299	TSSOP-EP MAX3288 MAX3298	NAME	FUNCTION
1	1			FAULT	Inverting Fault Indicator. See Table 1.
—	2, 16, 19	—	—	N.C.	No Connect
2	3	—		FAULT	Noninverting Fault Indicator. See Table 1.
3	4	2	2	POR	Power-On Reset. POR is a TTL-compatible output. See Figure 14.
4, 13, 19	5, 14, 22, 30	1, 6	1, 6	GND	Ground
5	6	_	_	EN	Enable TTL Input. Laser output is enabled only when EN is high and EN is low. If EN is left unconnected, the laser is disabled.
6	7	_	_	ĒN	Inverting Enable TTL Input. Laser output is enabled only when EN is low or grounded and EN is high. If EN is left unconnected, the laser is disabled.
7	8	_		PORDLY	Power-On Reset Delay. To extend the delay for the power-on reset circuit, connect a capacitor to PORDLY. See <i>Design</i> <i>Procedure</i> .

## Pin Description (continued)

	PIN							
QFN MAX3286 MAX3296	TQFP MAX3286 MAX3296	TSSOP-EP MAX3287 MAX3297 MAX3289 MAX3299	TSSOP-EP MAX3288 MAX3298	NAME	FUNCTION			
8	9	_	_	FLTDLY	Fault Delay Input. Determines the delay of the FAULT and FAULT outputs. A capacitor attached to FLTDLY ensures proper startup. (See <i>Typical Operating Characteristics.</i> ) FLTDLY = GND: holds FAULT low and FAULT high. When FLTDLY = GND, EN = high, $\overline{EN}$ = low, and V <sub>CC</sub> is within the operational range, the safety circuitry is inactive.			
9	10		_	LV	Low-Voltage Operation. Connect to GND for 4.5V to 5.5V operation. Leave open for 3.0V to 5.5V operation (Table 2).			
10, 22, 23, 26	11, 25, 26, 29	3, 11, 14	3, 11, 14	V <sub>CC</sub>	Supply Voltage			
11	12	4	4	IN+	Noninverting Data Input			
12	13	5	5	IN-	Inverting Data Input			
14	15	7	7	REF	Reference Voltage. A resistor connected at REF to MD determines the laser power when APC is used with common-cathode lasers.			
15	17	_		POL	Polarity Input. POL is used for programming the laser-pinning polarity (Table 4).			
16	18	_	_	POL	Inverting Polarity Input. POL is used for programming the laser-pinning polarity (Table 4).			
17	20	8	8	MD	Monitor Diode Connection. MD is used for automatic power control.			
18	21		9	MON	Laser Bias Current Monitor. Used for programming laser bias current in VCSEL applications.			
20	23	9		SHDNDRV	Shutdown Driver Output. Provides a redundant laser shutdown.			
21	24	10	10	BIASDRV	Bias-Controlling Transistor Driver. Connects to the base of an external PNP or NPN transistor.			

## Pin Description (continued)

	P	IN			
QFN MAX3286 MAX3296	TQFP MAX3286 MAX3296	TSSOP-EP MAX3287 MAX3297 MAX3289 MAX3299	TSSOP-EP MAX3288 MAX3298	NAME	FUNCTION
24	27	12	12	OUT+	Modulation-Current Output. See <i>Typical</i> Application Circuits.
25	28	13	13	OUT-	Modulation-Current Output. See <i>Typical Application Circuits</i> .
27	31	15	15	MODSET	Modulation-Current Set. The resistor at MODSET programs the temperature-stable component of the laser modulation current.
28	32	16	16	TC	Temperature-Compensation Set. The resistor at TC programs the temperature-increasing component of the laser modulation current.
EP	_	EP	EP	Exposed Pad	Ground. This must be soldered to the circuit board ground for proper thermal performance. See <i>Layout Considerations</i> .

## **Table 1. Typical Fault Conditions**

PIN	FAULT CONDITION
Vcc	$LV =$ open and $V_{CC} < 3V$ ; $LV =$ GND and $V_{CC} < 4.5V$
REF	$V_{\text{REF}} > 2.95V$
POL and POL	$POL = \overline{POL}$
MON	$V_{MON} < V_{CC}$ - 540mV
MD	$V_{MD} > 1.15 \times V_{MD(nom)},$ $V_{MD} < 0.85 \times V_{MD(nom)}$
EN and EN	$EN = low or open, \overline{EN} = high or open$
MODSET and TC	$V_{MODSET}$ and $V_{TC} \le 0.8V$

## Table 2. LV Operating Range

LV	OPERATING VOLTAGE RANGE (V)
Open	>3.0
Grounded	>4.5

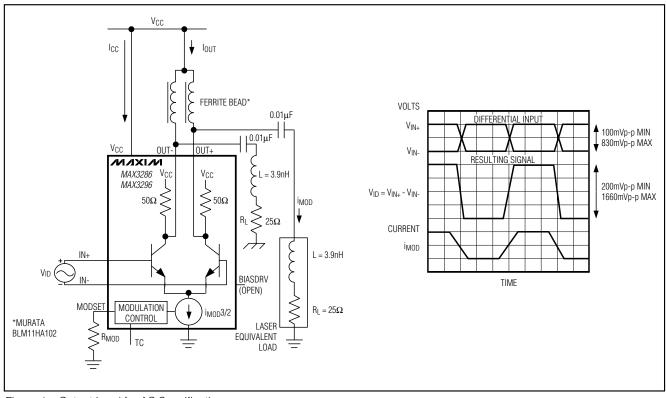


Figure 1a. Output Load for AC Specification

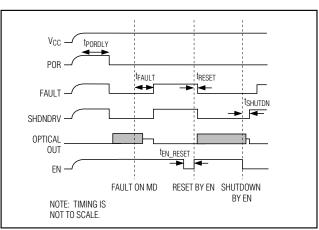


Figure 1b. Fault Timing

## **Detailed Description**

The MAX3286/MAX3296 series of laser drivers contain a bias generator with APC, laser modulator, power-on reset (POR) circuit, and safety circuitry (Figures 2a and 2b).

#### **Bias Generator**

Figure 3 shows the bias generator circuitry containing a power-control amplifier, controlled reference voltage, smooth-start circuit, and window comparator. The bias generator combined with an external PNP or NPN transistor provides DC laser current to bias the laser in a light-emitting state. When there is a monitor diode (MD) in the laser package, the APC circuitry adjusts the laser-bias current to maintain average power over tem-

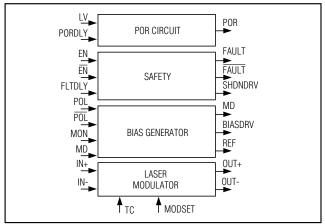


Figure 2a. Simplified Laser Driver Functional Diagram

perature and changing laser properties. The MD input is connected to the anode or cathode of a monitor photodiode or to a resistor-divider, depending on the specific application circuit. Three application circuits are supported: common-cathode laser with photodiode, common-cathode laser without photodiode, and commonanode laser with photodiode (as shown in the *Design Procedure*). The POL and POL inputs determine the laser pinning (common cathode, common anode) (Table 4).

The smooth-start circuitry prevents current spikes to the laser during power-up or enable; this ensures compliance with safety requirements and extends the life of the laser.

The power-control amplifier drives an external transistor to control the laser bias current. In a fault condition, the power-control amplifier's output is disabled (high

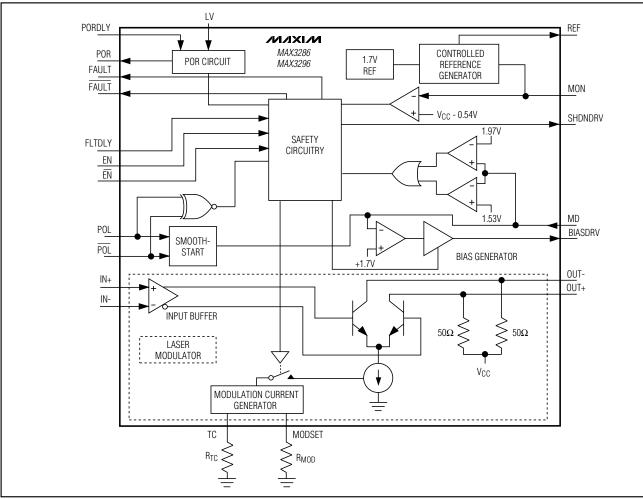


Figure 2b. Laser Driver Functional Diagram

impedance). This ensures that the PNP or NPN transistor is turned off, removing the laser-bias current. (See *Applications Information*.)

The REF pin provides a controlled reference voltage dependent upon the voltage at MON. The voltage at REF is  $V_{REF} = 2.65 - 2.25(V_{CC} - V_{MON})$ . A resistor connected at REF determines the laser power when APC is used with common-cathode lasers. See *Design Procedure* for setting the laser power.

#### Modulation Circuitry

The modulator circuitry consists of an input buffer, current generator, and high-speed current switch (Figure 4). The modulator drives up to 30mA of modulation current into a  $25\Omega$  load.

Many of the modulator performance specifications depend on the total modulator current (IOUT) (Figure 1a). To ensure good driver performance, the voltage at OUT+ and OUT- must not be less than V<sub>CC</sub> - 1V.

The amplitude of the modulation current is set with resistors at the MODSET and temperature coefficient (TC) pins. The resistor at MODSET ( $R_{MOD}$ ) programs the temperature-stable portion of modulation current, while the resistor at TC ( $R_{TC}$ ) programs the temperature-increasing portion of the modulation current. Figure 5 shows modulation current as a function of temperature for two extremes: RTC is open (the modulation current has zero temperature coefficient) and  $R_{MOD}$  is open (the modulation temperature coefficient is 4000ppm). Intermediate tempco values of modulation current can be obtained as described in the *Design Procedure*. Table 3 is the RTC and R<sub>MOD</sub> selection table.

#### **Safety Circuitry**

The laser driver can be used with two popular safety systems. APC maintains laser safety using local feedback. Safety features monitor laser driver operation and

TEMPOO	i <sub>MOD</sub> = 30mA		MOD = 30mA i <sub>MOD</sub> = 15mA			5mA
TEMPCO (ppm/°C)	R <sub>MOD</sub> (kΩ)	<b>Rтс</b> (kΩ)	R <sub>MOD</sub> (kΩ)	<b>Rтс</b> (kΩ)	R <sub>MOD</sub> (kΩ)	R <sub>TC</sub> (kΩ)
3500	26.7	1.69	53.6	3.65	162	11.5
3000	9.53	2.0	18.7	4.32	57.6	13.3
2500	5.76	2.49	11.3	5.23	34.8	16.2
2000	4.12	3.16	8.06	6.49	24.9	20.0
1500	3.24	4.32	6.19	8.87	19.1	26.7
1000	2.67	6.49	5.11	13.3	15.8	40.2
500	2.26	13.3	4.22	26.7	13.3	80.6

#### Table 3. RTC and RMOD Selection Table

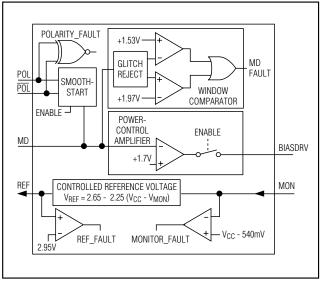


Figure 3. Bias Generator Circuitry

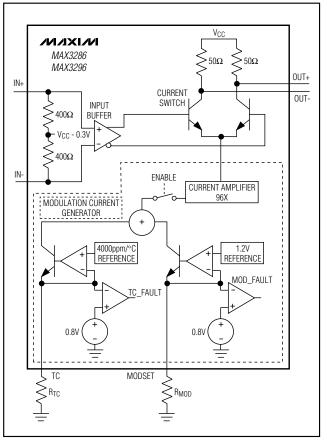


Figure 4. Laser Modulator Circuitry

MAX3286-MAX3289/MAX3296-MAX3299

# MAX3286-MAX3289/MAX3296-MAX3299

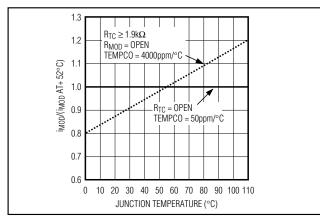
# 3.0V to 5.5V, 1.25Gbps/2.5Gbps LAN Laser Drivers

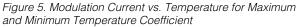
force a shutdown if a fault is detected. The shutdown condition is latched until reset by a toggle of EN,  $\overline{\text{EN}},$  or power.

Another safety system, Open Fiber Control (OFC), uses safety interlocks to prevent eye hazards. To accommodate the OFC standard, the MAX3286/MAX3296 series provide dual enable inputs and dual fault outputs.

The safety circuitry contains fault detection, dual enable inputs, latched fault outputs, and a pulse generator (Figure 6).

Safety circuitry monitors the APC circuit to detect unsafe levels of laser emission during single-point failures. A single-point failure can be a short to  $V_{CC}$  or GND, or between any two IC pins.





#### **Pulse Generator**

During startup, the laser is not emitting light and the APC loop is not closed, triggering a fault signal. To allow startup, an internal fault-delay pulse disables the safety system for a programmable period of time, allowing the driver to begin operation. The length of the pulse is determined by the capacitor connected at FLTDLY and should be set 5 to 10 times longer than the APC time constant. The internal safety features can be disabled by connecting FLTDLY to GND. Note that EN must be high, EN must be low, and V<sub>CC</sub> must be in the operational range for laser operation.

#### Fault Detection

The MAX3286/MAX3296 series has extensive and comprehensive fault-detection features. All critical nodes are monitored for safety faults, and any node voltage that differs significantly from its expected value results in a fault (Table 1). When a fault condition is detected, the laser is shut down. See *Applications Information* for more information on laser safety.

#### Shutdown

The laser drivers offer dual redundant bias shutdown mechanisms. The SHDNDRV output drives an optional external MOSFET semiconductor. The bias and modulation drivers have separate, internal disable signals.

#### Latched Fault Output

Two complementary FAULT outputs are provided with the MAX3286/MAX3296 series. In the event of a fault, these outputs latch until one of three events occurs:

1) The power is switched off, then on.

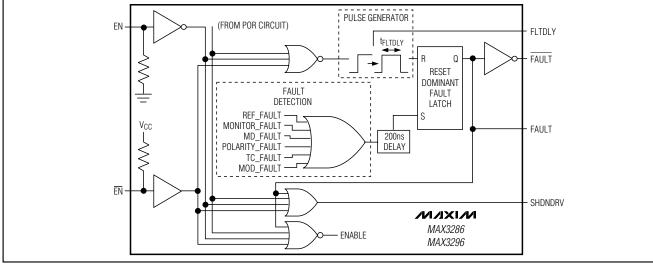


Figure 6. Simplified Safety Circuit Schematic

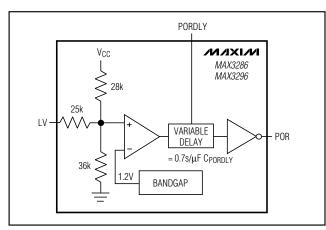


Figure 7. Power-On Reset Circuit

2) EN is switched low, then high.

3) EN is switched to high, then low.

#### **Power-On Reset (POR)**

Figure 7 shows the POR circuit for the MAX3286/ MAX3296 series devices. A POR signal asserts low when VCC is in the operating range. The voltage operating range is determined by the LV pin, as shown in Table 2. POR contains an internal delay to reject noise on VCC during power-on or hot-plugging. The delay can be extended by adding capacitance to the PORD-LY pin. The POR comparator includes hysteresis to improve noise rejection. The laser driver is shut down while VCC is out of the operating range.

#### Design Procedure

#### Select Laser

Select a communications-grade laser with a rise time of 260ps or better for 1.25Gbps, or 130ps or better for 2.5Gbps applications. To obtain the MAX3286/MAX3296s' AC specifications, the instantaneous output voltage at OUT+ must remain above V<sub>CC</sub> - 1V at all times. Select a high-efficiency laser that requires low modulation current and generates low-voltage swing at OUT+. Laser package inductance can be reduced by trimming the leads. Typical package leads have inductance of 25nH/in (1nH/mm); this inductance causes a larger voltage swing across the laser. A compensation filter network can also be used to reduce ringing, edge speed, and voltage swing.

#### **Programming the Modulation Current**

Resistors at the MODSET and TC pins set the amplitude of the modulation current. The resistor  $\mathsf{R}_{\text{MOD}}$  sets the temperature-stable portion of the modulation cur-

rent while the resistor RTC sets the temperatureincreasing portion of the modulation current.

To determine the appropriate temperature coefficient from the slope efficiency ( $\alpha$ ) of the laser, use the following equation:

Laser Tempco = 
$$\frac{\alpha_{70} - \alpha_{25}}{\alpha_{25}(70^{\circ}\text{C} - 25^{\circ}\text{C})} \times 10^{+6} \text{ [ppm/°C]}$$

where  $\boldsymbol{\alpha}$  is the slope of the laser output power to the laser current.

For example, suppose a laser has a slope efficiency  $\alpha_{25}$  of 0.021mW/mA at +25°C, which reduces to 0.018mW/mA at +70°C. Using the above equation will produce a laser tempco of -3175ppm/°C.

To obtain the desired modulation current and tempco for the device, the following two equations can be used to determine the required values of R<sub>MOD</sub> and R<sub>TC</sub>:

$$R_{TC} = \frac{0.21}{Tempco(i_{MOD})} - 250\Omega$$

$$R_{\text{MOD}} = \frac{(R_{\text{TC}} + 250\Omega)52 \times \text{Tempco}}{(0.19 - 48 \times \text{Tempco})} - 250\Omega$$

where Tempco = -Laser Tempco.

Figure 8a shows a family of curves derived from these equations. The straight diagonal lines depict constant tempcos. The curved lines represent constant modulation currents. If no temperature compensation is desired, Figure 8b displays a series of curves that show laser modulation current with respect to R<sub>MOD</sub> for different loads.

The following useful equations were used to derive Figure 8a and the equations at the beginning of this section. The first assumes  $R_L = 25\Omega$ .

$$i_{MOD} = 51 \times \left[ \frac{1.15}{R_{MOD} + 250\Omega} + \frac{1.06}{R_{TC} + 250\Omega} \times \\ \left( (1 + 4.0 \times 10^{-3} (T - 25^{\circ}C)) \right) \right] [A]$$

 $iMOD(70^{\circ}C) = iMOD(25^{\circ}C) + iMOD(25^{\circ}C)$  $(TEMPCO)(70^{\circ}C-25^{\circ}C)[A]$ 

#### **Programming the Bias Current/APC**

Three application circuits are described below: common-cathode laser with photodiode, common-cathode laser without photodiode, and common-anode laser

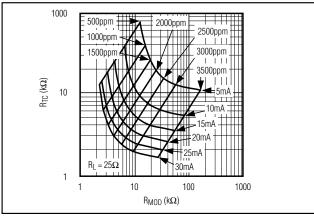


Figure 8a. RTC vs. RMOD for Various Conditions

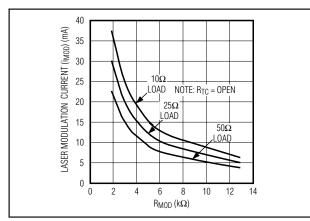


Figure 8b. Laser-Modulation Current vs. RMOD

with photodiode. The POL and POL inputs determine the laser pinning (common cathode, common anode) and affect the smooth-start circuits (Table 4).

#### Common Cathode with Photodiode (Optical Feedback)

In the common cathode with photodiode configuration, a servo control loop is formed by external PNP Q1, the laser diode, the monitor diode, R<sub>SET</sub>, and the power-control amplifier (Figure 9). The voltage at MD is stabilized to 1.7V. The monitor photodiode current (I<sub>D</sub>) is set by (V<sub>REF</sub> - V<sub>MD</sub>) / R<sub>SET</sub> = 0.95 / R<sub>SET</sub>. Determine the desired monitor current (I<sub>D</sub>), then select R<sub>SET</sub> = 0.95 / I<sub>D</sub>.

The APC loop is compensated by C<sub>BIASDRV</sub>. A capacitor must be placed from BIASDRV to V<sub>CC</sub> to ensure lownoise operation and to reject power-supply noise. The time constant governs how quickly the laser bias current reacts to a change in the average total laser current (I<sub>BIASDRV</sub> + i<sub>MOD</sub>). A capacitance of 0.1µF is sufficient to obtain a loop time constant in excess of 1µs, provided that R<sub>DEG</sub> is chosen appropriately. Resistor R<sub>DEG</sub> may be necessary to ensure the APC loop's stability when low bias currents are desired.

The voltage across RDEG should not be any larger than 250mV at maximum bias current.

The discrete components used with the common cathode with photodiode configuration are as follows:

RSET = 0.88 / ID

CBIASDRV =  $0.1\mu$ F (typ)

RDEG = 0.25 / IBIAS(MAX)

## Table 4. POL Pin Setup for Each Laser Configuration Type

DEVICE	POL	POL	DESCRIPTION	LASER PINNING			
MAX3286/MAX3296	VCC	GND		**			
MAX3287/MAX3297	_		Common cathode with photodiode				
MAX3286/MAX3296	VCC	GND		<u> </u>			
MAX3288/MAX3298	_		Common cathode without photodiode				
MAX3286/MAX3296	GND	VCC		Vcc			
MAX3289/MAX3299	_		Common anode with photodiode				
MAX3286/MAX3296	VCC	VCC	Not allowed; fault occurs	_			
MAX3286/MAX3296	GND	GND	Not allowed; fault occurs				



Q1 = general-purpose PNP,  $\beta$  >100, ft > 5MHz

B1 = ferrite bead (see *Bias Filter* section)

M1 = general-purpose PMOS device (optional)

**Common Cathode with Current Feedback** In the common-cathode configuration with current feedback, a servo control loop is formed by an external PNP transistor (Q1), R<sub>MON</sub>, the controlled-reference voltage block, R<sub>SET</sub>, R<sub>MD</sub>, and the power-control amplifier (Figure 10). The voltage at MD is stabilized to 1.7V. The voltage at MON is set by the resistors R<sub>SET</sub> and R<sub>MD</sub>. As in the short-wavelength configuration, a 0.1µF CBIASDRV connected between BIASDRV and V<sub>CC</sub> is sufficient to obtain approximately a 1 $\mu s$  APC loop time constant. This improves power-supply noise rejection.

To select the external components:

1) Determine the required laser bias current:

IBIAS = ITH + IMOD / 2

2) Select RMD and RSET.

Maxim recommends RsET = 1kΩ, RMD = 5kΩ, which results in VCC - VMON  $\approx$  250mV.

3) Select R<sub>MON</sub> where R<sub>MON</sub> = 250mV / I<sub>BIAS</sub>, assuming R<sub>SET</sub> = 1k $\Omega$  and R<sub>MD</sub> = 5k $\Omega$ .

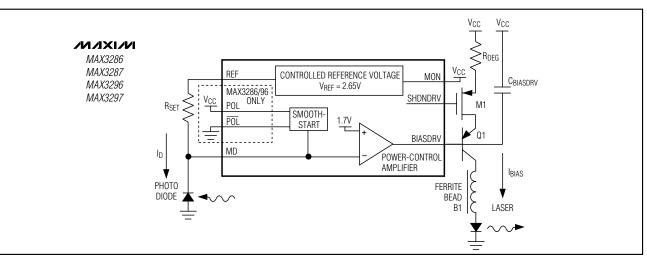


Figure 9. Common-Cathode Laser with Photodiode

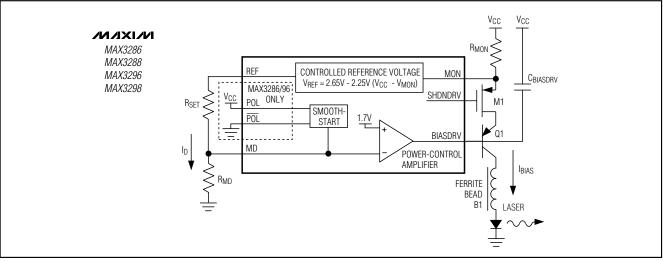


Figure 10. Common Cathode with Current Feedback (PNP Configuration)

The relationship between laser bias current and RMON is shown in Figure 11. The remaining discrete components used with the common cathode without photodiode configuration are as follows:

Q1 = general-purpose PNP,  $\beta$  >100, ft > 5MHz

B1 = ferrite bead (see *Bias Filter* section)

M1 = general-purpose PMOS device (optional)

 $CBIASDRV = 0.1 \mu F (typ)$ 

#### Common Anode with Photodiode

In the common-anode configuration with photodiode, a servo control loop is formed by an external NPN transistor (Q1), the laser diode, the monitor diode, R<sub>SET</sub>, and the power-control amplifier. The voltage at MD is stabilized to 1.7V. The monitor photodiode current is set by I<sub>D</sub> = V<sub>MD</sub> / R<sub>SET</sub> (Figure 12). Determine the desired monitor current (I<sub>D</sub>), then select R<sub>SET</sub> = 1.7V / I<sub>D</sub>.

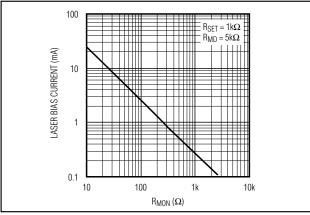


Figure 11. Common Cathode without Photodiode Laser

CBIASDRV and a degeneration resistor (RDEG) must be connected to the bias transistor (in this case NPN) to obtain the desired APC loop time constant. This improves power-supply (and ground) noise rejection. A capacitance of  $0.1\mu F$  is sufficient to obtain time constants of up to 5µs in most cases. The voltage across RDEG should not be larger than 250mV at maximum bias current.

The discrete components used with the common anode with photodiode configuration are summarized as follows:

$$R_{SET} = 1.7 / I_D$$

 $C_{BIASDRV} = 0.1 \mu F (typ)$ 

 $R_{DEG} = 0.25 / I_{BIAS(MAX)}$ 

Q1 = general-purpose NPN,  $\beta$  > 100, ft > 5MHz

B1 = ferrite bead (see *Bias Filter* section)

M1 = general-purpose PMOS (optional)

#### **Programming POR Delay**

A capacitor may be added to PORDLY to increase the delay for which POR will be asserted low (meaning that V<sub>CC</sub> is within the operational range) when powering up the part.

The delay will be approximately:

$$t = \frac{C_{PORDLY}}{(1.4)10^{-6}} [s]$$

See Typical Operating Characteristics.

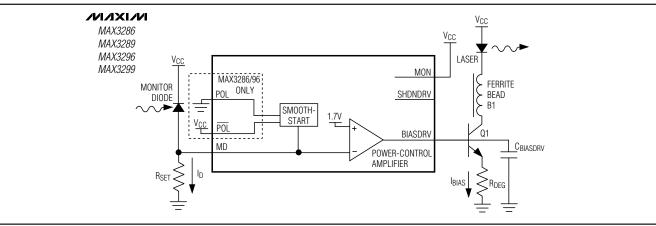


Figure 12. Common Anode with Photodiode



#### Designing the Bias Filter and Output Pullup Beads

To reduce deterministic jitter, add a ferrite-bead inductor between the collector of the biasing transistor and either the anode or cathode of the laser, depending on type (see *Typical Operating Characteristics*). Use a ferrite-bead inductor with an impedance >100 $\Omega$  between f = 10MHz and f = 2GHz, and a DC resistance < 3 $\Omega$ . Maxim recommends the Murata BLM11HA102SG. These inductors are also desirable for tying the OUT+ and OUT- pins to V<sub>CC</sub>.

#### Designing the Laser-Compensation Filter Network

Laser package inductance causes the laser impedance to increase at high frequencies, leading to ringing, overshoot, and degradation of the output eye pattern. A lasercompensation filter network can be used to reduce the output load seen by the laser driver at high frequencies, thereby reducing output ringing and overshoot.

The compensation components (R<sub>COMP</sub> and C<sub>COMP</sub>) are most easily determined by experimentation. Begin with R<sub>COMP</sub> =  $25\Omega$  and C<sub>COMP</sub> = 2pF. Increase C<sub>COMP</sub> until the desired transmitter eye is obtained (Figure 13).

#### **Quick Shutdown**

To reduce laser shutdown time, a FET device can be attached to SHDNDRV as shown in Figure 10. This will provide a typical laser power shutdown time of less than  $10\mu s$ .

## **Applications Information**

#### Laser Safety and IEC 825

The International Electrotechnical Commission (IEC) determines standards for hazardous light emissions from fiber optic transmitters. IEC 825 defines the maximum light output for various hazard levels. The MAX3286/MAX3296 series provides features that facilitate compliance with IEC 825.

A common safety requirement is single-point fault tolerance, whereby one unplanned short, open, or resistive connection does not cause excess light output. When these laser drivers are used, as shown in the *Typical Operating Circuits*, the circuits respond to faults as listed in Table 5.

Using these laser drivers alone does not ensure that a transmitter design is compliant with IEC 825. The entire transmitter circuit and component selections must be considered. Customers must determine the level of fault tolerance required by their applications, recognizing that Maxim products are not designed or authorized for use as components in systems intended for surgical implant

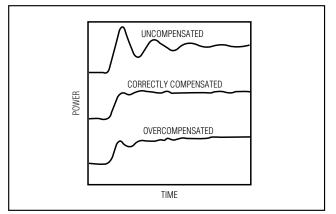


Figure 13. Laser Compensation

into the body, for applications intended to support or sustain life, or for any other application where the failure of a Maxim product could create a situation where personal injury or death may occur.

#### **Layout Considerations**

The MAX3286/MAX3296 series comprises high-frequency products. Their performance largely depends upon the circuit board layout.

Use a multilayer circuit board with a dedicated ground plane. Use short laser package leads placed close to the modulator outputs. Power supplies must be capacitively bypassed to the ground plane with surface-mount capacitors placed near the power-supply pins.

The dominant pole of the APC circuit is normally located at BIASDRV. To prevent a second pole in the APC (that can lead to oscillations), ensure that parasitic capacitance at MD is minimized.

#### **Common Questions**

Laser output is ringing or contains overshoot. This is often caused by inductive laser packaging. Try reducing the length of the laser leads. Modify the compensation components to reduce the driver's output edge speed (see *Design Procedure*). Extreme ringing can be caused by low voltage at the OUT± pins. This may indicate that pullup beads or a lower modulation current are needed.

*Low-frequency oscillation on the laser output.* This is more prevalent at low temperatures. The APC may be oscillating. Try increasing the value of CBIASDRV or increasing the value of RDEG. Ensure that the parasitic capacitance at the MD node is kept very small (<10pF).

The APC is not needed. Connect FLTDLY to ground to disable fault detection. Connect MD to REF and MON to V\_CC. BIASDRV and SHDNDRV can be left open.



## Table 5. Circuit Response to Various Single-Point Faults

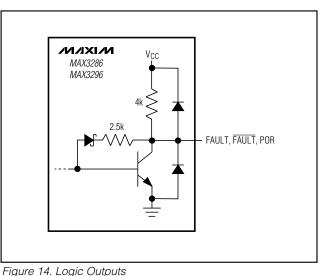
PIN NAME	CIRCUIT RESPONSE TO OVERVOLTAGE OR SHORT TO V <sub>CC</sub>	CIRCUIT RESPONSE TO UNDERVOLTAGE OR SHORT TO GROUND	
FAULT	Does not affect laser power.	Does not affect laser power.	
FAULT	Does not affect laser power.	Does not affect laser power.	
POR	Does not affect laser power. Does not affect laser power.		
PORDLY	Does not affect laser power. Fault state* occurs.		
EN	Normal condition for circuit operation.	Fault state* occurs.	
ĒN	Fault state* occurs.	Normal condition for circuit operation.	
LV	Does not affect laser power.	Fault state* occurs if V <sub>CC</sub> is less than +4.5V.	
POL	If POL is a TTL HIGH, a fault state* occurs; other- wise, the circuit is in normal operation.	If POL is a TTL LOW, a fault state* occurs; other- wise, the circuit is in normal operation.	
POL	If POL is a TTL HIGH, a fault state* occurs; other- wise, the circuit is in normal operation.	If POL is a TTL LOW, a fault state* occurs; other- wise, the circuit is in normal operation.	
MON (also MAX3288/98)	In common cathode without photodiode configura- tion, a fault state* occurs; otherwise, does not affect laser power.	Fault state* occurs.	
SHDNDRV (also MAX3287/97/ 89/99)	Does not affect laser power. If optional FET is used, the laser output is shut off.	Does not affect laser power.	
FLTDLY	Any fault that occurs cannot be reset. Does not affect laser power.	Does not affect laser power.	
IN+, IN-	Does not affect laser power.	Does not affect laser power.	
REF	Fault state* occurs.	In common-cathode configurations, a fault state* occurs; otherwise, does not affect laser power.	
MD	Fault state* occurs.	Fault state* occurs.	
BIASDRV	In common-cathode configurations, the laser bias current is shut off. In common anode, high laser power triggers a fault state.* Shutdown occurs if a shutdown FET (M1) is used. If shutdown FET is not used, other means must be used to prevent high laser power.	In common-anode configurations, the laser bias current is shut off. In common cathode, high laser power triggers a fault state.* Shutdown occurs if a shutdown FET (M1) is used (Figures 9, 10).	
OUT+, OUT-	Does not affect laser power.	Does not affect laser power.	
MODSET	Does not affect laser power.	Fault state* occurs.	
TC	Does not affect laser power.	Fault state* occurs.	

\* A fault state will assert the FAULT pins, disable the modulator outputs, disable the bias output, and assert the SHDNDRV pin.

*The modulator is not needed.* Leave TC and MODSET open. Connect IN+ to VCC, IN- to REF, and leave OUT+ and OUT- open.

#### Wirebonding Die

The MAX3286/MAX3296 series uses bondpads with gold metalization. Make connections to the die with gold wire only, using ball-bonding techniques. Wedge bonding is not recommended. Bondpad size is 4mil square. Die thickness is typically 15mils (0.38mm).



**Interface Models** Figures 14–18 show typical input/output models for the MAX3286/MAX3296 series of laser drivers. If dice are used, replace the package parasitic elements with bondwire parasitic elements.

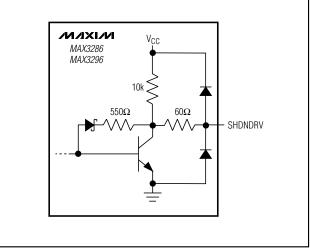


Figure 15. SHDNDRV Output

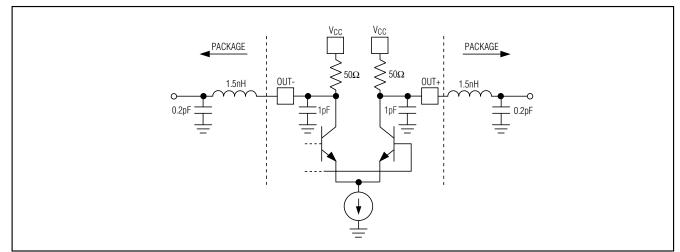


Figure 16. Modulator Outputs

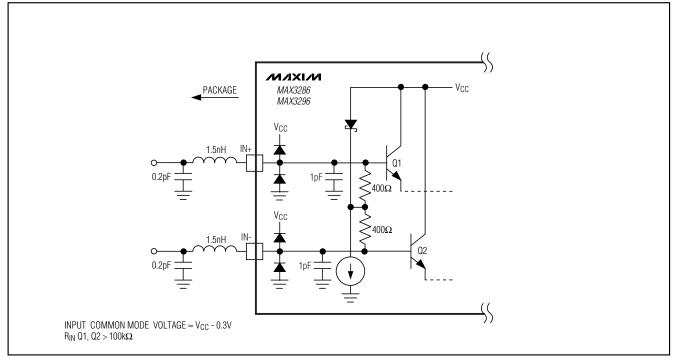


Figure 17. Data Inputs

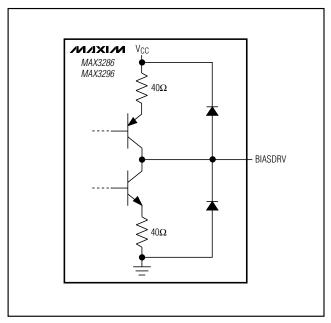
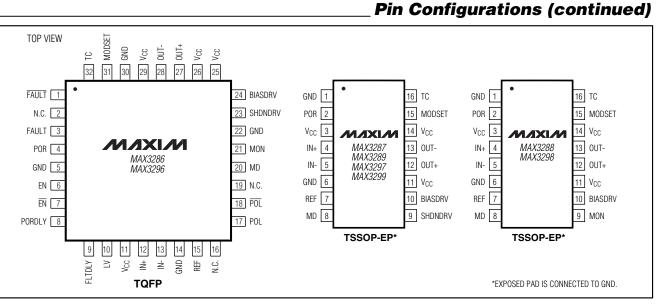


Figure 18. BIASDRV Output



## Selector Guide

DATA RATE/DEVICE		LASER CONFIGURATION			
1.25Gbps	2.5Gbps	COMMON ANODE WITH PHOTODIODE	COMMON CATHODE WITH PHOTODIODE	COMMON CATHODE WITH PHOTODIODE	PACKAGE
		Longwave	Shortwave or VCSEL	VCSEL	
MAX3286	MAX3296	✓	1	1	32 TQFP/28 QFN/dice
MAX3287	MAX3297		1		16 TSSOP-EP
MAX3288	MAX3298			1	16 TSSOP-EP
MAX3289	MAX3299	1			16 TSSOP-EP



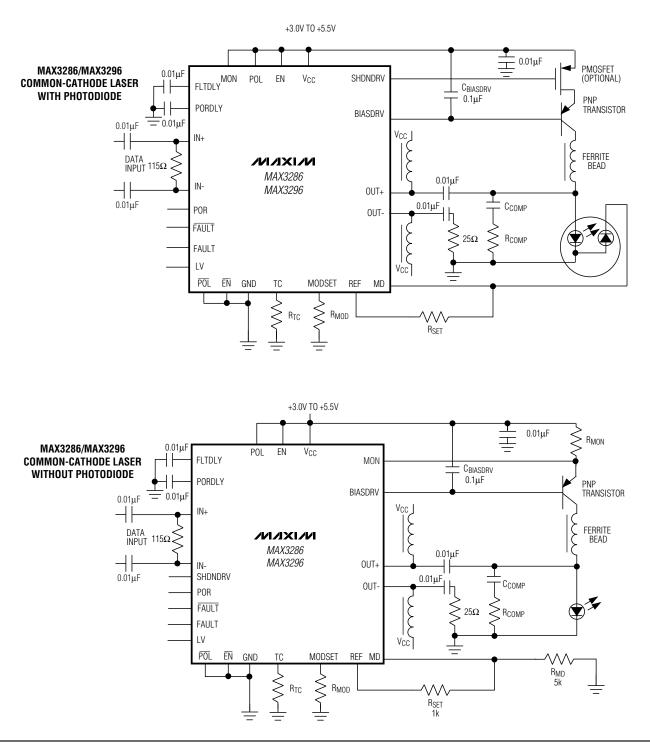
## Ordering Information (continued)

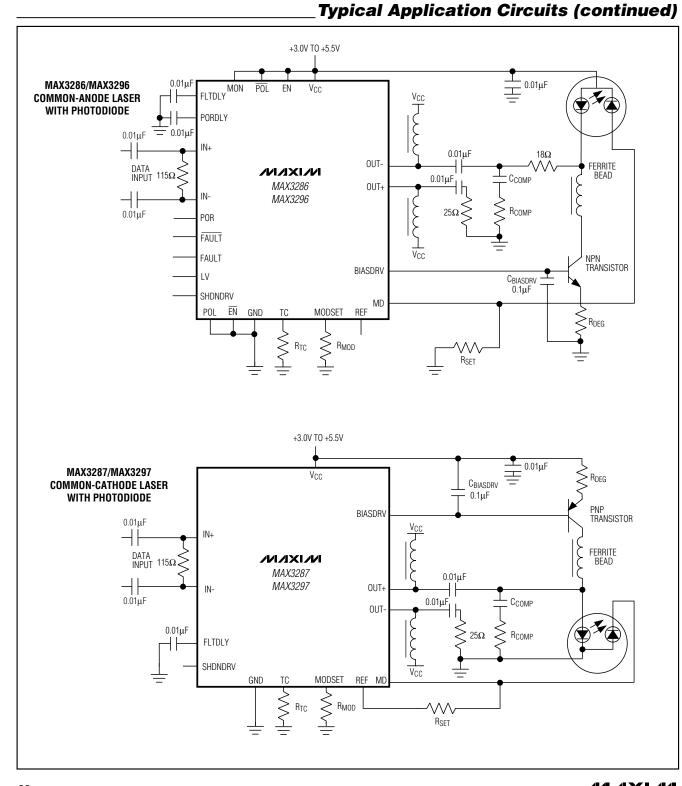
PART	TEMP. RANGE	PIN- PACKAGE
MAX3287CUE	0°C to +70°C	16 TSSOP-EP**
MAX3288CUE	0°C to +70°C	16 TSSOP-EP**
MAX3289CUE	0°C to +70°C	16 TSSOP-EP**
MAX3296CGI	0°C to +70°C	28 QFN (5mm × 5mm)**
MAX3296CHJ	0°C to +70°C	32 TQFP (5mm × 5mm)
MAX3296C/D	0°C to +70°C	Dice*
MAX3297CUE	0°C to +70°C	16 TSSOP-EP**
MAX3298CUE	0°C to +70°C	16 TSSOP-EP**
MAX3299CUE	0°C to +70°C	16 TSSOP-EP**

\*Dice are designed to operate from  $T_J = 0^{\circ}C$  to +110°C, but are tested and guaranteed only at  $T_A = +25^{\circ}C$ . \*\*Exposed pad.



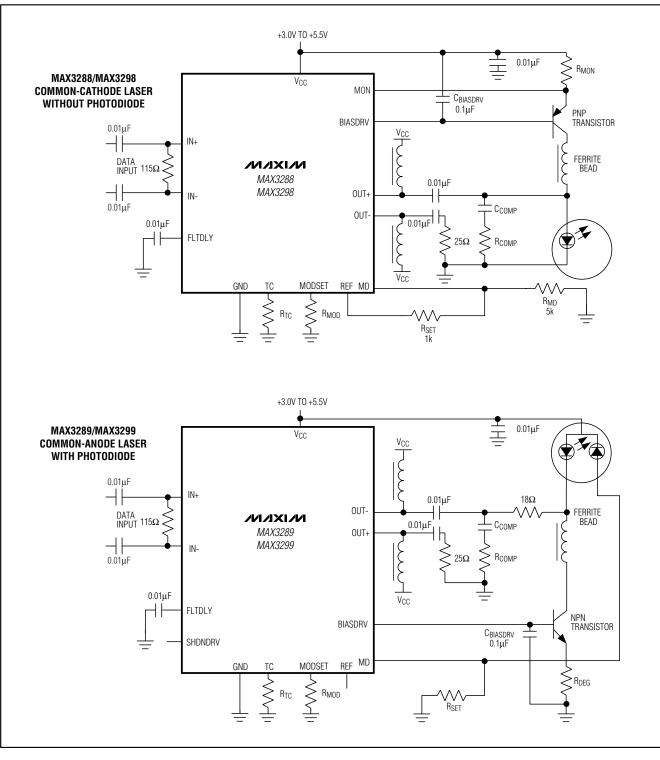
## **Typical Application Circuits**



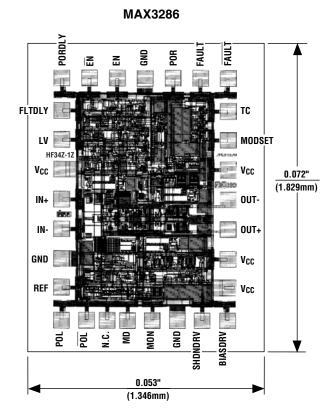


M/IXI/M

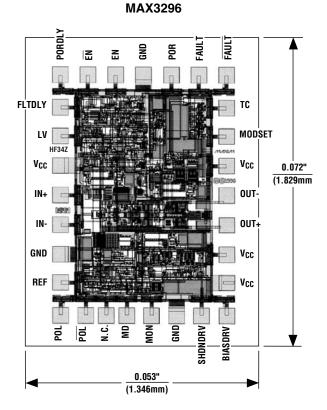
## **Typical Application Circuits (continued)**



Chip Topographies



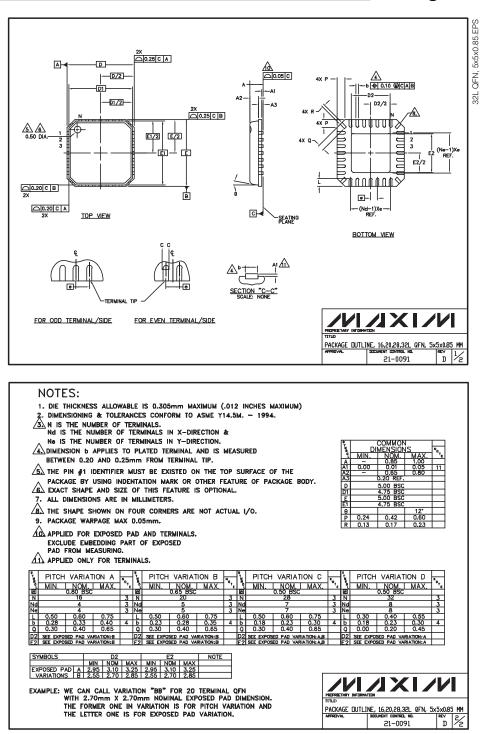
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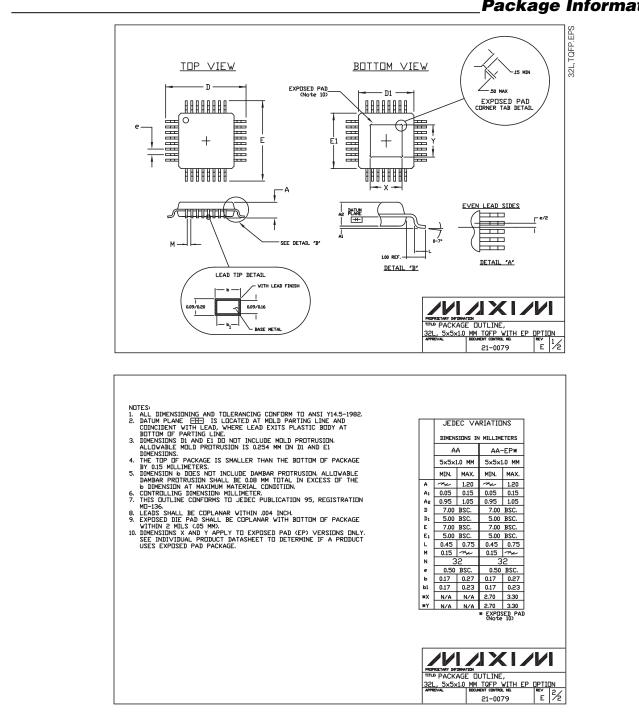
TRANSISTOR COUNT: 1154 SUBSTRATE CONNECTED TO GND

MAX3286-MAX3289/MAX3296-MAX3299

### **Package Information**

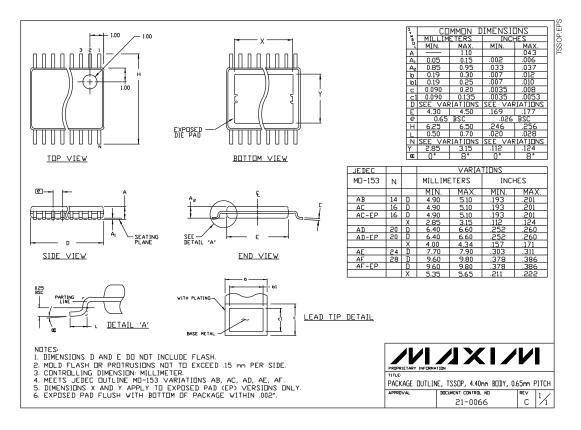


MAX3286-MAX3289/MAX3296-MAX3299



**Package Information** 

## \_Package Information (continued)



MAX3286-MAX3289/MAX3296-MAX3299

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